

## Equivalence between condensation and boiling in a Lennard-Jones fluid

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Condensation and boiling are phase transitions highly relevant to industry, geology, and atmospheric science. These phase transitions are initiated by the nucleation of a drop in a supersaturated vapor and of a bubble in an overstretched liquid, respectively. The surface tension between both phases, liquid and vapor, is a key parameter in the development of such nucleation stage. Whereas the surface tension can be readily measured for a flat interface, there are technical and conceptual limitations to obtain it for the curved interface of the nucleus. On the technical side, it is quite difficult to observe a critical nucleus in experiments. From a conceptual point of view, the interfacial free energy depends on the choice of the dividing surface, being the surface of tension the one relevant for nucleation. We bypass the technical limitation by performing simulations of a Lennard-Jones fluid where we equilibrate critical nuclei (both drops and bubbles). Regarding the conceptual hurdle, we find the relevant cluster size by searching the radius that correctly predicts nucleation rates and nucleation free energy barriers when combined with Classical Nucleation Theory. With such definition of the cluster size we find the same value of the surface tension for drops and bubbles of a given radius. Thus, condensation and boiling can be viewed as two sides of the same coin. Finally, we combine the data coming from drops and bubbles to obtain, via two different routes, estimates of the Tolman length, a parameter that allows describing the curvature dependence of the surface tension in a theoretical framework.

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### I. INTRODUCTION

Understanding first-order phase transitions is of great importance to many fields, ranging from biology [1] to atmospheric science [2], physics [3], geology [4], and industry [5,6].

In the absence of impurities or external surfaces, first-order phase transitions start with the emergence of a nucleus of the stable phase in the bulk of the parent metastable phase [7,8]. A nucleus is “critical” if it is big enough so that it has a 50% chance to either grow or redissolve.

Although the emerging phase is more stable, the presence of an unfavourable interface between the nucleus and the parent phase can delay to a great extent the phase transition. Thus, for instance, alkane vapors can be saturated thousands of times over their vapor pressure before condensation takes place [9], alkane liquids can be substantially superheated above the boiling temperature [10–12], or liquid water can be supercooled up to  $\sim 60$  K below melting until it freezes [13–16].

Therefore, the surface tension,  $\gamma$ , or the free energy per unit area between both phases, plays a key role in the development of first-order phase transitions. Whereas  $\gamma$  can be readily measured for a flat interface at equilibrium—at least between fluid phases [17]—it cannot be directly probed for curved interfaces, which is the relevant case for nucleation. Moreover, the fact that critical nuclei are nanoscopic objects makes it very difficult to observe them in experiments, let alone measure their  $\gamma$ . The usual strategy is to infer  $\gamma$  by combining a theoretical description of nucleation with measurements of the nucleation rate (the number of nuclei that

appear per unit of time and volume) [7,17–19]. This approach relies on the validity of theoretical approximations that are difficult to assess.

Computer simulations do have access to the time and length scales relevant for the observation of critical nuclei. However, whereas the methodology and theoretical framework for computing  $\gamma$  for flat interfaces is very well established [20–29], that for curved interfaces is still under development [30–32]. One of the key issues is that  $\gamma$  for curved interfaces depends on the location of the interface, which can be defined in different ways [32,33]. The current situation is that the dependence of  $\gamma$  with the curvature of the interface is contradictory between different groups [18,30–32,34–44].

In this work we address fundamental questions regarding the liquid-vapor interface with computer simulations. It has been shown in different simulation works that spherical nuclei can be equilibrated at constant volume and temperature in finite systems [35,44–53]. Recently, we showed with simulations of bubbles [54] and crystals [55] that nuclei thus equilibrated are critical, in agreement with Density Functional Theory (DFT) predictions [56,57]. On the other hand, we have extensively developed recently the so-called Seeding method [58–61] to study nucleation phenomena. This method consists in obtaining with simulations the properties of critical clusters and “plugging” them in the Classical Nucleation Theory (CNT) formalism [62–65] to obtain predictions of the nucleation rate and of the  $\gamma$ -curvature dependence. This approach has been successful for a wide range of

systems [54,58,59,61,66–70], and we use it here to study condensation. In particular, we apply Seeding at constant volume both to condensation and to cavitation for a Lennard-Jones model.

Since Seeding relies on CNT, it is necessary to validate it by comparing its predictions with rigorous calculations that do not rely on such a framework. We do so by computing nucleation rates via Umbrella Sampling (US) [71,72] and direct brute force simulations [73] as well as by testing the consistency of the  $\gamma$ -curvature dependence obtained via Seeding with the value for a flat interface.

All consistency tests are successfully passed for our Seeding simulations provided that the nucleus surface is identified with that where the density is the average between the density of both phases (“equidensity” surface). Therefore, we identify the equidensity surface with the surface of tension. On the other hand, we directly compare the condensation of liquid drops in a supersaturated vapor with the cavitation of vapor bubbles in an overstretched liquid. We find that, for a given temperature, drops and bubbles of the same radius have the same  $\gamma$  when using the equidensity definition of the surface of tension. Finally, we estimate the Tolman length [74], a parameter useful to predict the  $\gamma$ -curvature dependence, via two different routes, as recently proposed in Ref. [55].

## II. SIMULATION DETAILS

The Lennard-Jones model potential, as well as the simulation details, are the same as in our previous work [54,70]. In particular, we study the truncated and force-shifted Lennard-Jones (TSF-LJ) potential [75], a model for which the vapor-liquid transition has been previously investigated [70,75–77]:

$$U_{\text{TSF-LJ}}(r) = U_{\text{LJ}}(r) - U_{\text{LJ}}(r_c) - (r - r_c)U'_{\text{LJ}}(r_c), \quad (1)$$

where  $U_{\text{LJ}}(r)$  is the standard 12-6 Lennard-Jones potential and  $U'_{\text{LJ}}(r)$  is its first derivative. The interaction potential is truncated and shifted at  $r_c = 2.5\sigma$ , where  $\sigma$  is the particle’s diameter and  $\epsilon$  the depth of the untruncated Lennard-Jones potential. Unless otherwise specified, all magnitudes in this work are given in Lennard-Jones reduced units [54]. Thus, the reported temperatures are reduced by  $\epsilon/k_B$ , distances by  $\sigma$ , densities by  $\sigma^{-3}$ , pressures by  $\epsilon/\sigma^3$ , times by  $\tau = \sqrt{m\sigma^2/\epsilon}$  (where  $m$  is the particle mass), interfacial free energies by  $\epsilon/\sigma^2$ , and nucleation rates by  $1/(\tau\sigma^3)$ .

We use cubic boxes with periodic boundary condition and the molecular dynamics (MD) LAMMPS package [78] to perform all simulations of this work. The equations of motion are integrated with a leap-frog algorithm [79].

In the MD Seeding simulations we used a time step of 0.0012. The system was kept at constant temperature using the Nosé-Hover thermostat [80] with a relaxation time of 0.46.

For the MD simulations used within the US scheme we set the time step for the integration of the motion equations to 0.0012. The relaxation times for the Nosé-Hover thermostat and barostat were 0.46 and 1.6, respectively.

All simulations are carried out at  $T = 0.785$ . The coexistence pressure at such a temperature for the model is  $p_{\text{coex}} = 0.0267$ . We determined this value, refined with respect to that of 0.026 previously published [75], by running

long ( $4 \times 10^5 \tau$ ) MD *NVT* (i.e. in the canonical ensemble) simulations with an elongated box ( $50 \times 17 \times 17$ ) where the vapor and the liquid were put in contact at the temperature of interest. The average pressure normal to the interface in such a simulation corresponds to  $p_{\text{coex}}$ .

## III. SEEDING OF CONDENSATION

This work is based on a recent publication where we demonstrate how to compute bubble nucleation rates in an overstretched Lennard-Jones fluid by equilibrating critical bubbles in the *NVT* ensemble, an approach we call “*NVT*-Seeding” [54]. The Seeding method, originally developed to study crystal nucleation [58–61], and more recently applied to vapor cavitation [54,70,81], consists in combining CNT [62–65] with computer simulations to estimate nucleation free energy barrier heights,  $\Delta G_c$ , interfacial free energies,  $\gamma$ , and, most importantly, nucleation rates,  $J$ .

According to CNT, the Gibbs free energy barrier for the nucleation of a spherical liquid drop is given by the following expression:

$$\Delta G = \gamma A - V \Delta p, \quad (2)$$

where  $V$  and  $A$  are the volume and the area of the drop, respectively. By maximizing Eq. (2) assuming a spherical drop shape one obtains both the height of the nucleation free energy barrier,

$$\Delta G_c = \frac{2\pi R_c^3 \Delta p}{3}, \quad (3)$$

where  $R_c$  is the critical droplet radius and  $\Delta p$  is the pressure difference between the interior of the drop and the surrounding vapor, and the number of particles in the critical drop,

$$N_c = (32\pi \rho_l \gamma^3)/(3\Delta p^3), \quad (4)$$

where  $\rho_l$  is the critical drop number density and  $\gamma$  is the liquid-vapor surface tension. By substituting in the equation above  $N_c$  by the droplet volume ( $4/3\pi R_c^3$ ) times  $\rho_l$  one recovers the Laplace equation:

$$\Delta p = \frac{2\gamma}{R_c}. \quad (5)$$

This derivation shows that the Laplace equation, which is valid when the droplet surface is located at the surface of tension, is implicit in CNT. Consequently,  $R_c$  should be identified with the radius of tension,  $R_s$ . This is an important point that we will use later in the paper.

The CNT prediction for the nucleation rate of drops is given by [7]

$$J = A_0 \rho_{\text{vap}} \exp\left(-\frac{\Delta G_c}{k_B T}\right), \quad (6)$$

where  $k_B$  is the Boltzmann constant,  $\rho_{\text{vap}}$  is the density of the vapor phase that multiplied by  $\exp(-\frac{\Delta G_c}{k_B T})$  gives the number density of critical clusters, and  $A_0$  is a kinetic prefactor.

$A_0$  is computed as the product of the Zeldovich factor,  $Z$ , and the rate of attachment to the critical nucleus,  $f^+$  [7,63]:

$$A_0 = Z f^+. \quad (7)$$

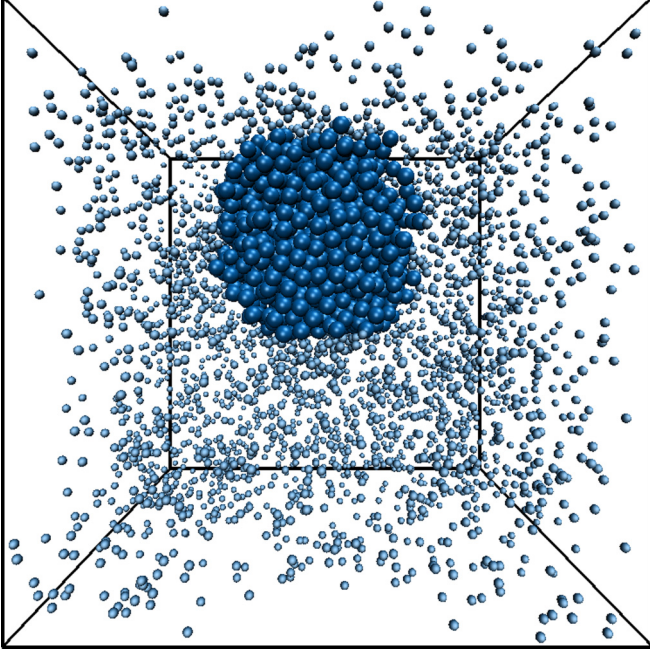


FIG. 1. Snapshot of a critical drop equilibrated in the  $NVT$  ensemble at  $T = 0.785$  surrounded by supersaturated vapor. The droplet radius is about 6.8, and the density of the surrounding vapor 0.0550.

$Z$  takes into account the establishment of a steady state, and, according to CNT, is given by [7,62,63]

$$Z = \sqrt{\frac{|\Delta G(N)''|_{N_c}}{2\pi k_B T}} = \sqrt{\frac{\Delta p}{6\pi k_B T \rho_l N_c}} = \sqrt{\frac{\Delta p}{8\pi^2 k_B T \rho_l^2 R_c^3}}, \quad (8)$$

where  $N_c$  is the number of particles in the drop and  $|\Delta G_c(N)''|_{N_c}$  is the curvature of  $\Delta G(N)$  evaluated at the barrier top.

The attachment rate,  $f^+$ , can be estimated by multiplying the collision frequency of the vapor per unit of wall area given by the kinetic theory of gases (ktg) by the area of the critical bubble:

$$f_{\text{ktg}}^+ = \sqrt{\frac{k_B T}{2\pi m}} \left( \frac{6\sqrt{\pi} N_c}{\rho_l} \right)^{2/3}, \quad (9)$$

where the subscript “ktg” stresses the fact that this expression of the attachment rate is based on the kinetic theory of gases. Combining this equation with Eqs. (8), (4), and (5), the following kinetic prefactor is obtained:

$$A_0^{\text{ktg}} = \sqrt{\frac{\Delta p R_c}{\pi m}} \frac{\rho_{\text{vap}}}{\rho_l}. \quad (10)$$

The equations above are quite powerful, because only  $R_c$ ,  $\Delta p$ , and the density of both phases are required to obtain key nucleation parameters such as free energy barriers, interfacial free energies, and nucleation rates. The Seeding method consists in performing simulations of a cluster of the stable phase surrounded by the metastable phase (a liquid drop surrounded by supersaturated vapor in our case as shown in Fig. 1) to compute  $R_c$ ,  $\Delta p$ ,  $\rho_l$ , and  $\rho_{\text{vap}}$  in order to get “cheap”

estimates of  $\Delta G_c$ ,  $\gamma$ , and, most importantly,  $J$  through the expressions above.

The main drawback of Seeding is that the definition of  $R_c$  is not unique. Therefore, the resulting free energy barrier depends on the specific definition of  $R_c$ . This contrasts with rigorous simulation methods like US [73,82] or with theoretical approaches like DFT [83–85] where the nucleation free energy does not depend on the criterion chosen to measure the nucleus size, which can be estimated *a posteriori* via, e.g., the nucleation theorem [86–88] (although in the particular case of DFT an approximate functional needs to be proposed so that the results do also contain approximations). To assess the suitability of our choice to compute  $R_c$  we complement Seeding with US simulations.

#### A. $R_c$ , $\Delta p$ , $\rho_l$ , and $\rho_{\text{vap}}$

We use the  $NVT$  ensemble to run the simulations of the drops given that in such an ensemble critical nuclei are naturally equilibrated and stabilized for long times [54,55]. We equilibrate drops in 10 different systems. The edge of the cubic simulation box,  $L$ , and the total number of particles in each system,  $N_T$ , are reported in Table I. A large number of particles are used to minimize finite-size effects [52,54,89]. Each system was simulated for about  $10^3$  Lennard-Jones times of equilibration and  $2 \times 10^5$  of production.

To prepare the initial configuration we cut a spherical liquid drop from a bulk liquid simulation and insert it in a bulk vapor box removing the overlapping vapor particles. The liquid drop is cut with a certain tentative radius, but the precise number of particles in each phase is not crucial given that equilibrium is reached along the course of the  $NVT$  simulation.

From a simulation of a drop surrounded by supersaturated vapor one can obtain an average radial density profile starting from the center of the drop as that shown in Fig. 2 (to find the drop center in each configuration we use a strategy similar to that described in our previous work [54] consisting in this case in identifying the maxima of density profiles computed along each cartesian coordinate). Following Refs. [54,70], we obtain  $R_c$  from such a density profile as the distance at which the density is average between the liquid and the vapor plateaux. This is indicated with a vertical dashed line in Fig. 2. We refer to this way of obtaining  $R_c$  as the “equidensity” criterion. The  $R_c$ ’s thus obtained in our  $NVT$ -Seeding simulations are also reported in Table I. Other definitions of  $R_c$  are in principle as valid as the equidensity criterion [70,84,85]. We argue later in the paper that our  $R_c$  definition is a good one because it makes Seeding predictions consistent with independent calculations of  $\gamma$ ,  $J$ , or  $\Delta G_c$ .

To get  $\Delta p = p_l - p_{\text{vap}}$  we obtain first the vapor density,  $\rho_{\text{vap}}$ , by counting the number of particles outside a sphere concentric with the drop but with a larger radius (we use a sphere radius  $7\sigma$  larger than that of the drop, but we have checked for a few selected cases that any value beyond  $\sim 5\sigma$  gives the same result).  $\rho_{\text{vap}}$  is given by the number of particles outside the sphere divided by the  $L^3$  minus the sphere volume. We then use the bulk vapor equation of state to infer  $p_{\text{vap}}$  from  $\rho_{\text{vap}}$ . We report  $p_{\text{vap}}$  and  $\rho_{\text{vap}}$  in Table I. We have checked for all studied systems that  $p_{\text{vap}}$  coincides with the overall virial

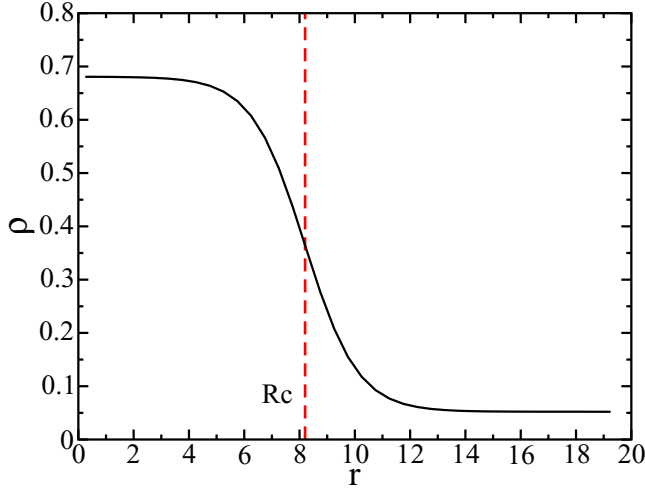


FIG. 2. Density profile of a critical drop equilibrated in the  $NVT$  ensemble at  $T = 0.785$  surrounded by supersaturated vapor. The droplet radius, indicated by a red vertical line, is given by the point at which  $\rho(r)$  takes an average value between both plateaux (equidensity criterion). The density profile corresponds to the system labeled as IV in Table I.

pressure of the system. On the other hand,  $p_l$  is obtained, as in our previous work [54,70], by assuming equal chemical potential between the critical drop and the surrounding vapor:

$$\int_{p_{\text{coex}}}^{p_{\text{vap}}} \frac{1}{\rho_{\text{vap}}(p)} dp = \int_{p_{\text{coex}}}^{p_l} \frac{1}{\rho_l(p)} dp, \quad (11)$$

where  $p_{\text{coex}}$  is the coexistence pressure and  $\rho_{\text{vap}}(p)$  and  $\rho_l(p)$  are the bulk vapor and bulk liquid number densities at pressure  $p$ , respectively. In Table I we report  $p_l$  and  $\Delta p$  for all studied systems. Once  $p_l$  is known,  $\rho_l$ , also reported in the table, can be easily computed from the bulk liquid equation of state. In all cases, this computation of  $\rho_l$ , based on the equality of chemical potential between both phases, is consistent with that obtained from the density profiles. For instance, for system IV we get  $\rho_l = 0.0680$ , which is fully consistent with the first plateau observed in the density profile shown in Fig. 2. This means that the mechanical pressure and the thermodynamic pressure inside the drop coincide, a matter of current debate for solid-liquid nucleation [90].

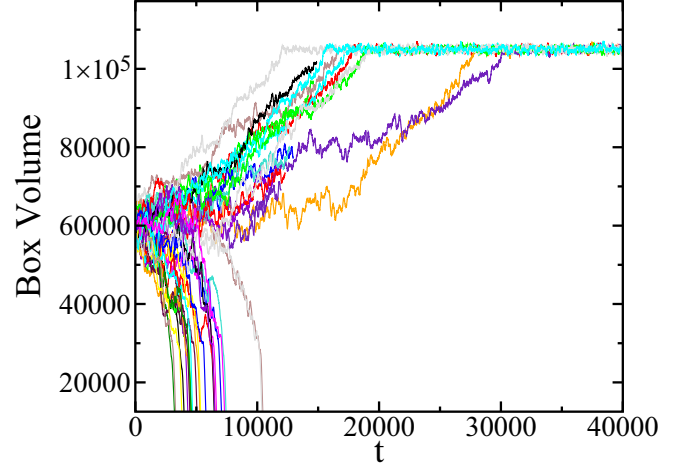


FIG. 3. Box volume vs time in  $NpT$  simulations starting from 40 configurations taken from the  $NVT$ -Seeding simulation labeled IX in Table I. The imposed pressure is the average virial pressure of the  $NVT$ -Seeding run.

There has been much simulation, theoretical, and experimental work devoted to study of the formation of nuclei confined at constant volume [32,44,48,91–99]. In Refs. [54,55] we showed with simulations that nuclei equilibrated in the  $NVT$  ensemble are critical because they have equal chances to grow or shrink when simulated in the  $NpT$  (i.e. isothermal isobaric ensemble) at the same temperature and at the average pressure along the  $NVT$  run. Based on this result, we opted to study here drop nucleation in the  $NVT$  ensemble, where statistics is better because clusters remain stable for very long times [54]. Stabilizing nuclei to gain time to study their properties is something quite desirable. An alternative strategy to the use of constant volume simulations is to pin the nucleus to a heterogeneous solid substrate [100].

Despite having already shown the equivalence between stable ( $NVT$ ) and critical ( $NpT$ ) nuclei for cavitation [54], we check here for one of the  $NVT$ -Seeding simulations if the drops equilibrated at constant volume and temperature do correspond to a Gibbs free energy maximum. In Fig. 3 we show the evolution of the box volume in  $NpT$  simulations started from 40 independent configurations gathered along the  $NVT$ -Seeding trajectory labeled IX in Table I. The imposed pressure is the average virial pressure along the  $NVT$ -Seeding

TABLE I.  $NVT$ -Seeding data for the different drops studied in this work at  $T = 0.785$ .

Label	$L$	$N_T$	$\rho_l$	$\rho_{\text{vap}}$	$p_l$	$p_{\text{vap}}$	$\Delta p$	$R_c$	$\gamma$	$\Delta G_c/(k_B T)$	$A_0^{\text{ktg}}$	$A_0^{\text{af}}$	$\log_{10}(J)$
I	38.019	3774	0.6833	0.05690	0.09279	0.03161	0.0612	5.86	0.1792	32.8	0.028		−17.1
II	39.160	4291	0.6811	0.05496	0.0846	0.03092	0.0537	6.82	0.1831	45.5	0.028		−22.6
III	39.160	4373	0.6801	0.05414	0.08095	0.03063	0.0503	7.15	0.1800	49.2	0.027		−24.2
IV	39.160	4510	0.6797	0.05384	0.07961	0.03052	0.0491	7.48	0.1835	54.8	0.027	0.030	−26.6
V	39.160	4623	0.6792	0.05342	0.07769	0.03037	0.0473	7.79	0.1843	59.7	0.027		−28.8
VI	39.160	4796	0.6782	0.05277	0.07468	0.03013	0.0446	8.20	0.1827	65.5	0.027	0.036	−31.3
VII	39.160	4964	0.6783	0.05269	0.07432	0.03010	0.0442	8.49	0.1878	72.3	0.027		−34.2
VIII	39.160	5163	0.6776	0.05216	0.07181	0.02991	0.0419	8.86	0.1856	77.8	0.027		−36.6
IX	39.160	5435	0.6771	0.05176	0.06989	0.02976	0.0401	9.30	0.1865	86.0	0.026		−40.2
X	85.264	34519	0.6761	0.05105	0.06638	0.02949	0.0369	9.99	0.1843	98.2	0.026		−45.5



run. Roughly, in 50% of the cases the box expands (the drop dissolves), and in the other half of the cases the box shrinks (the drop grows). This result supports the use of  $NVT$  to study drop condensation in the same manner that we used for bubble cavitation and crystal nucleation [54,55]. Furthermore, the equivalence between clusters equilibrated at constant volume and critical nuclei has been recently proven with DFT theoretical arguments for crystallization (see supplementary material of Ref. [57]).

Having computed  $R_c$ ,  $\Delta p$ ,  $\rho_{\text{vap}}$ , and  $\rho_l$  we have everything needed to obtain  $\gamma$ ,  $\Delta G_c$  and  $J$  according to the equations presented in Sec. III. We report the values for these variables in Table I and plot them in Figs. 4(a)–4(c) versus the vapor pressure with black dots. In the following section we comment on each of these graphs.

## B. $\gamma$ , $\Delta G_c$ , and $J$

### 1. $\gamma$

As shown in Fig. 4(a) the prediction we obtain from Seeding is that  $\gamma$  decreases as the vapor supersaturation increases. This trend is in agreement with previous work [35,47]. Accordingly, using the capillarity approximation (i.e., that  $\gamma$  is pressure independent) would be erroneous. The green square in Fig. 4(a) corresponds to the surface tension at coexistence [70] obtained through the pressure tensor [101] in an  $NVT$  simulation of a liquid and a vapor at contact. The trend of the Seeding data is fully consistent with the coexistence value, as shown by the linear fit in the figure. This is a good consistency test, although the  $\gamma$  values provided by Seeding could still be incorrect despite the fact that they extrapolate correctly to coexistence. Therefore, a test for Seeding predictions away from coexistence is needed.

### 2. $\Delta G_c$

To further test our Seeding results we compare  $\Delta G_c$  obtained with Seeding with that computed via US. In Fig. 4(b), where we plot  $\Delta G_c$  versus the vapor pressure, black solid dots correspond to Seeding and red ones to US (details on US calculations are described in Sec. IV). Whereas Seeding predictions rely on the validity of CNT and on a proper definition of  $R_c$ , US calculations are rigorous and independent on the criterion to identify the nucleus size [73]. On the other hand Seeding is much “cheaper” than US from a computational point of view. As a matter of fact, Seeding has access to much higher nucleation barriers than US. The accordance between Seeding and US shown in Fig. 4 is excellent, which gives us great confidence in Seeding predictions. The choice of the equidensity surface to identify the drop radius has proven correct. If we use another criterion, such as the Gibbs (equimolar) dividing surface, the agreement between Seeding and US deteriorates [empty black symbols in Fig. 4(b)]. To compute  $R_e$ , the radius associated with the Gibbs dividing surface, we use  $N_T = N_l + N_{\text{vap}}$  where  $N_l = 4/3\pi R_e^3 \rho_l$  and  $N_{\text{vap}} = [V_T - (4/3\pi R_e^3)]\rho_{\text{vap}}$ , where  $V_T$  is the volume of the simulation box and the densities  $\rho_l$  and  $\rho_{\text{vap}}$  are obtained as described in Sec. III A.

In a recent publication on cavitation (nucleation of bubbles instead of drops) we compared the performance of differ-

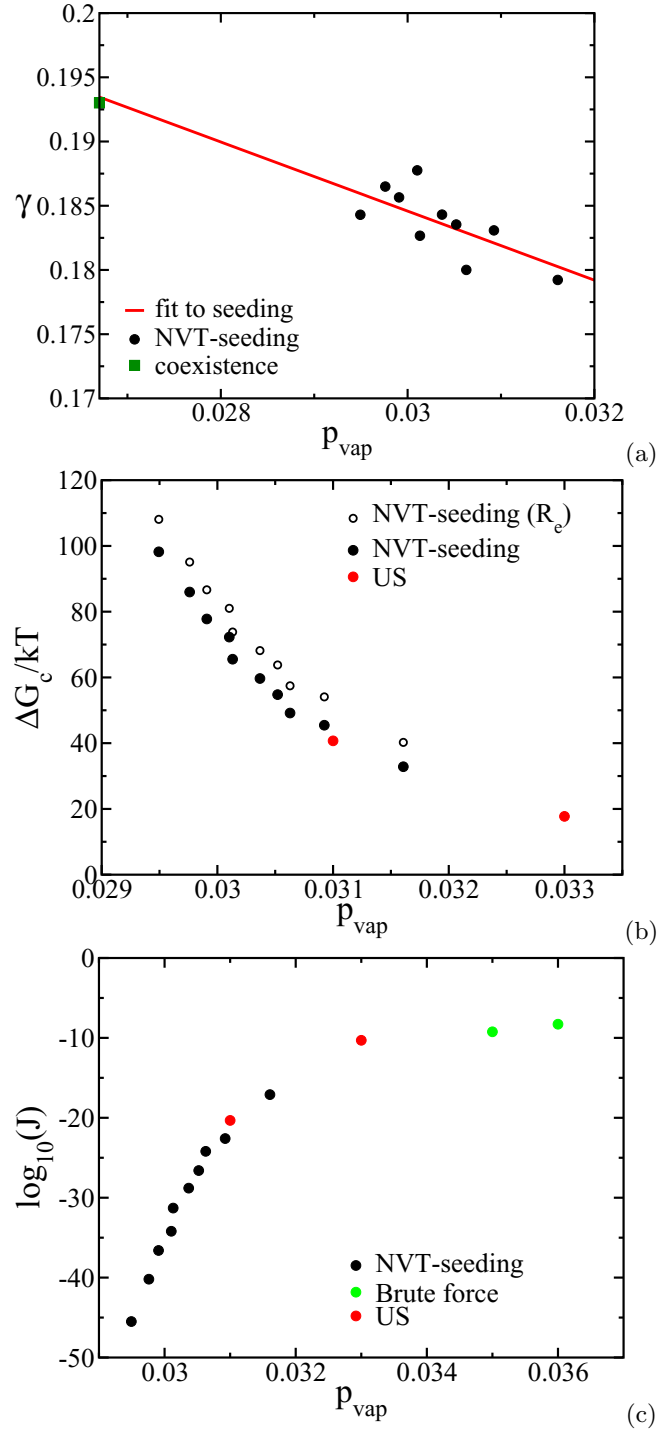


FIG. 4. (a)  $\gamma$  vs vapor pressure obtained from  $NVT$ -Seeding data of droplets surrounded by supersaturated vapor. The surface tension at coexistence ( $p = 0.0267$ ) is included [70]. (b)  $\Delta G_c$  vs vapor pressure.  $NVT$ -Seeding and US data are compared. Empty black symbols correspond to Seeding predictions when the Gibbs dividing (equimolar), instead of the equidensity, surface is employed to identify the cluster radius. (c) Nucleation rate vs vapor pressure as obtained from  $NVT$ -Seeding, US, and spontaneous nucleation.

ent criteria to identify the cluster radius and found that the equidensity criterion also made Seeding predictions consistent with other rigorous calculations [70]. Therefore, identifying

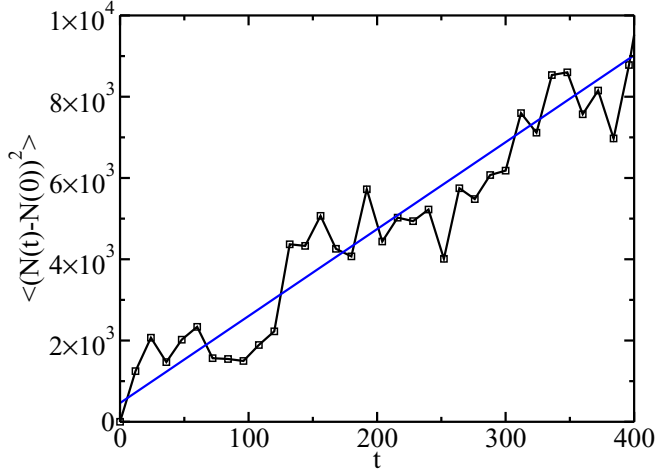


FIG. 5. Time dependence of the mean-squared deviation of the number of particles in the critical drop for system VI in Table I. Half the slope of this plot gives the attachment rate according to Eq. (12).

the critical drop radius with the equidensity distance seems to be quite general for condensation-evaporation transitions.

### 3. $J$

Once  $\Delta G_c$  is known computing  $J$  via Eq. (6) is quite straightforward. The kinetic prefactor  $A_0$  given by the kinetic theory of gases, Eq. (10), depends on parameters we already have under control:  $\Delta p$ ,  $R_c$ , and the density of both phases. The values of  $A_0$  computed via Eq. (10),  $A_0^{\text{ktg}}$ , are reported in Table I.

These  $A_0$  values are approximate since they rely on the validity of the kinetic theory of gases to estimate the attachment rate (see Sec. III). We therefore have to check  $A_0^{\text{ktg}}$  by computing the attachment rate with an alternative approach. Following the work by Auer and Frenkel [102], the attachment rate can be computed from the diffusion of  $N$ , the number of particles in the liquid drop, around the critical drop [102]:

$$f_{\text{af}}^+ = \frac{\langle (N(t) - N(0))^2 \rangle_{N_c}}{2t}, \quad (12)$$

where the average is performed over several trajectories starting from a critical drop configuration. The “af” subscript stresses the fact that this expression of the attachment rate is based on the work by Auer and Frenkel.

To compute  $N$  we follow Ref. [103]. We count as neighbors all particles within a 1.625 distance of a tagged particle. Particles with eight or more neighbors are labeled as “liquid.” Two liquid particles belong to the same drop if their mutual distance is less than 1.625. An example of the calculation of  $f^+$  according to Eq. (12) is illustrated in Fig. 5. Typically,  $\langle (N(t) - N(0))^2 \rangle_{N_c}$  is obtained by averaging 20  $NpT$  runs started from independent configurations of the critical drop, coming either from  $NVT$ -Seeding or from US simulations (see Sec. IV). In these runs, the pressure is fixed to the virial value of the simulations where the critical clusters were previously equilibrated. According to Eq. (12), the slope of Fig. 5 divided by 2 gives  $f^+$ . Multiplying such  $f^+$  by the Zeldovich factor we get an estimate of the kinetic prefactor,  $A_0^{\text{af}}$ , that does not

TABLE II. Data corresponding to the brute force calculations.

Label	$N_T$	$\langle V \rangle$	$p_v$	$\rho_v$	$\log_{10}(J)$
BF-1	4000	57 145	0.035	0.0700	−9.235
BF-2	4000	53 456	0.036	0.0748	−8.287

rely on the kinetic theory of gases.  $A_0^{\text{af}}$  is reported in Table I for a couple of critical clusters generated with  $NVT$ -Seeding (systems IV and VI).  $A_0^{\text{af}}$  is very close to  $A_0^{\text{ktg}}$ . This agreement suggests the validity of the kinetic theory of gases to estimate the attachment rate and makes the theoretical framework that supports the Seeding technique quite powerful given that, since  $A_0^{\text{ktg}}$  can be used, only  $R_c$ ,  $\Delta p$ , and the density of both phases are required to get accurate estimates of  $J$  in a wide range of orders of magnitude. Note in Fig. 4(c) that Seeding (black dots) has access to  $J$  values many orders of magnitude lower than US (red dots).

The green dots in Fig. 4(c) correspond to rate estimates obtained in brute force  $NPT$  molecular simulation runs performed at high supersaturations where condensation occurs spontaneously from an unseeded vapor. In such cases the nucleation rate can be estimated as  $J = 1/(t\langle V \rangle)$ , where  $\langle V \rangle$  is the average volume before nucleation and  $t$  is the nucleation time averaged over a number of independent trajectories (typically 20 in our case).  $N_T$ ,  $V$ , the vapor pressure and density, and  $J$  for the two states where we studied spontaneous condensation are reported in Table II. In Fig. 4(c) we show that  $J$  estimates from Seeding and from spontaneous nucleation are consistent with each other, which further indicates the ability of Seeding to predict nucleation rates. It is worth mentioning here that  $NVT$ -Seeding and spontaneous nucleation are complementary techniques. On the one hand, the former does not have access to such high supersaturations given the difficulty to equilibrate small clusters in the  $NVT$  ensemble [54,55]. That said, it would be nonsense to use Seeding where nucleation occurs spontaneously in a straightforward manner. On the other hand, spontaneous nucleation is limited to a narrow window of nucleation rates (that enabled by computational time), whereas Seeding has access to extremely low rates.

We would like to end this section by discussing finite-size effects, which could be present if a nucleus sees its replica through periodic boundary conditions. On the one hand, we made sure that the density of the outer phase reaches a plateau before  $L/2$  by looking at radial density profiles such as that shown in Fig. 2. On the other hand, we note that the box side of system X is more than twice than those of the other systems. By looking at Figs. 4(a), 4(b), and 4(c) one can see that the results from system X are fully consistent with those inferred from the other systems, which strongly supports the absence of noticeable finite-size effects in our simulations.

## IV. UMBRELLA SAMPLING

As previously indicated, to validate the Seeding results we used the US technique. We followed Refs. [103,104] to compute  $\Delta G_c$  for two different vapor pressures:  $p = 0.031$  and  $p = 0.033$ . Details on the simulation box size and number

TABLE III. Data corresponding to the US calculations.

Label	$L$	$N_T$	$\Delta G_c/(k_B T)$	$A_0^{\text{af}}$	$\log_{10}(J)$
US-1	39.112	4000	17.7	0.041	-10.3
US-2	38.501	4000	40.7	0.039	-20.3

of particles in the systems used to perform the US calculations are given in Table III.

The free energy associated with the formation of an  $N$  particle cluster drop can be obtained from

$$\Delta G(N) = -k_B T \ln[P(N)], \quad (13)$$

where  $P(N)$  is the probability distribution of  $N$ . Our criterion to compute  $N$  is described in Sec. III B 3. It is important to note that even though different criteria may give different  $N$  for a given configuration, the height of an US free energy barrier does not depend on the criterion to determine the cluster size [73]. Therefore, contrary to what happens in Seeding, the US method does not depend on the specific criterion to determine the nucleus size. This is why it is important to validate the Seeding method with other techniques such as US.

With conventional  $NpT$  simulations at the selected pressures  $P(N)$  can be sampled only up to  $N \sim 40$  while the critical cluster is much larger in this regime. To sample the rest of the free energy barrier a biasing potential,  $U_{\text{bias}}$ , is added to the original Hamiltonian:

$$U_{\text{bias}} = \frac{1}{2} k_{\text{bias}} (N - N_0)^2, \quad (14)$$

where  $N_0$  controls the cluster size around which the sampling will be centered and  $k$  the width of such sampling. Tens of overlapping sampling “windows” centered at different  $N_0$  values are required to reconstruct the whole free energy barrier. The effect of the bias potential on the calculation of the free energy barrier is removed as follows [71]:

$$\Delta G(N) = -k_B T \ln \left\langle \frac{\chi_N}{e^{-U_{\text{bias}}/(k_B T)}} \right\rangle + C, \quad (15)$$

where  $\chi_N$  is the fraction of clusters with  $N$  particles that appear within a certain window and  $C$  is a constant. The constant is obtained by gluing together the first part of the energy barrier evaluated without the biasing potential [Eq. (13)] with the rest of the windows. The result is the whole free energy barrier.

To compute each window we use the hybrid Molecular Dynamics–Monte Carlo scheme labeled as HMC(nM- $NpT$ )/US in Ref. [104]. From the starting configuration, random velocities are assigned to every particle according to a Maxwell-Boltzmann distribution, and a short ( $\Delta t$  19.2 Lennard-Jones times) MD simulation is run for generating a new configuration, which is accepted with probability  $\min[1, \exp\{-[U_{\text{bias}}(\Delta t) - U_{\text{bias}}(0)]/(k_B T)\}]$ . In the case of either acceptance or rejection new random velocities are assigned at the beginning of each short MD cycle. For each window, 10 000 of such cycles were performed for equilibration and 60 000 to obtain the free energy barrier. We used  $k_{\text{bias}} = 0.04 k_B T$  in the biasing potential [Eq. (14)], which gives an acceptance rate of  $\sim 25\%$ .

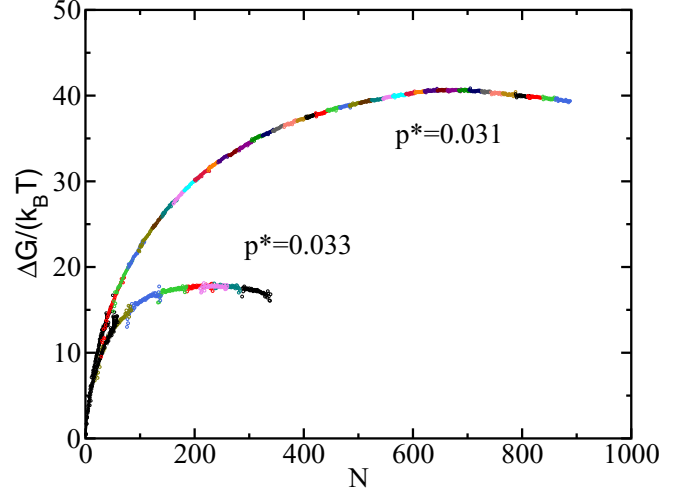


FIG. 6. Free energy for two different pressures ( $p = 0.031$  and  $p = 0.033$ ) versus the number of particles in the drop as obtained from US calculations. The different colors represent the different windows performed.

In Fig. 6 we plot both free energy barriers, where  $\Delta G_c = 17.7 k_B T$  for  $p = 0.033$  and  $\Delta G_c = 40.7 k_B T$  for  $p = 0.031$  (also reported in Table III). As already discussed, the agreement between US and Seeding is excellent [see Fig. 4(b)].

Additionally, we compute the kinetic prefactor  $A_0^{\text{af}}$  [Eq. (7)] to obtain the nucleation rate [Eq. (6)]. To do that, we launch tens of unbiased trajectories from independent configurations at the barrier top in order to compute the attachment rate via Eq. (12). The Zeldovich factor [Eq. (8)] can be obtained by numerically calculating the curvature of  $\Delta G(N)$  at the barrier top. We report  $A_0^{\text{af}}$  thus calculated and the corresponding  $J$  in Table III. As previously discussed,  $J$  from US is fully consistent with that coming from Seeding [see Fig. 4(c)].

In summary, we have compared Seeding, which relies on the theoretical assumptions by CNT and  $ktg$  and depends on the criterion employed to determine the cluster size, with US, which does not have these limitations. We have obtained an excellent agreement between both techniques. This is very good news because Seeding is much more efficient than US and has access to much lower values of the nucleation rate.

## V. CONDENSATION VERSUS BOILING

### A. Comparison for a given $R_c$

We have studied quite recently the nucleation of bubbles for the same Lennard-Jones model employed here [54]. Since the study was performed at the same temperature, the question that naturally arises is whether bubbles and drops with the same radius have the same interfacial properties. To establish the comparison we have repeated the analysis performed in Ref. [54] because in that work we used 0.026 as the coexistence pressure instead of 0.0267. We took the 0.026 value from a paper published more than a decade ago [75]. However, we have recomputed more carefully the coexistence pressure at  $T = 0.785$  and obtain  $p = 0.0267$  instead, which is the value we use in this work. The difference is subtle, but given

TABLE IV. *NVT*-Seeding data for the different bubbles studied in this work at  $T = 0.785$ .

Label	$L$	$N_T$	$\rho_{\text{vap}}$	$\rho_l$	$p_{\text{vap}}$	$p_l$	$\Delta p$	$R_c$	$\gamma$	$\Delta G_c/(k_B T)$	$A_0^{BK}$	$\log_{10}(J)$
I	36.731	30795	0.03765	0.6453	0.02365	-0.02601	0.0497	7.35	0.1826	52.7	0.341	-23.5
II	36.731	30342	0.03834	0.6484	0.02398	-0.01914	0.0431	8.50	0.1832	70.6	0.342	-31.3
III	36.731	29760	0.03875	0.6501	0.02419	-0.01503	0.0392	9.53	0.1869	90.6	0.345	-40.0
IV	36.731	29034	0.03907	0.6514	0.02433	-0.01191	0.0362	10.52	0.1906	112.5	0.348	-49.5
V	36.731	28147	0.03949	0.6530	0.02453	-0.00776	0.0323	11.50	0.1857	131.1	0.344	-57.6
VI	36.731	27082	0.03972	0.6539	0.02464	-0.00558	0.0302	12.45	0.1881	155.7	0.346	-68.3

that the pressure inside the nucleating phase is obtained by integrating from the coexistence pressure [see Eq. (11)], it is very important to use an accurate value for the latter.

The simulation data for different bubbles equilibrated at  $T = 0.785$  in the *NVT* ensemble are reported in Table IV. The values of  $R_c$  corresponding to each system (obtained with the equidensity criterion as discussed in Sec. III A and in Ref. [54]) are very close to those recently reported by ourselves [54]. However, the values of  $\Delta p$  here reported are not identical to those of Ref. [54] due to the coexistence pressure issue discussed above. In Fig. 7(a) we plot  $\Delta p$  versus  $1/R_c$  for bubbles and drops at  $T = 0.785$ . Drops and bubbles of the same size have the same  $\Delta p$ , which is perhaps the most important result of the paper. Note that, for a given  $R_c$ , the pressures of the external and the internal phases are not the same if one compares cavitation and condensation. What is the same is the pressure difference between the internal and the external phases. For instance, let us focus on the case of drop VII and bubble II, both with  $R_c \approx 8.5$ . In Fig. 8 we

compare their radial density profiles. The density of the liquid inside the drop is different from that of the liquid outside the bubble. Also, the density of the vapor inside the bubble is different from that of the vapor outside the drop. The bubble is surrounded by a liquid of pressure  $-0.01914$  whereas the drop by a vapor of pressure  $0.0301$ : the pressures of the external phases do not even have the same sign. The bubble and the drop also have very different pressures:  $0.02398$  and  $0.07432$ , respectively. Despite the fact that the external and the internal pressures are very different,  $\Delta p$  is not:  $0.043$  and  $0.044$  for the bubble and the drop, respectively.

According to the Laplace equation, that  $\Delta p(R_c)$  is the same for drops and bubbles, implies that  $\gamma$  also must be the same regardless of the identity of the internal and the external phases. In Fig. 7(b) we plot  $\gamma$  versus  $1/R_c$  for bubbles and drops and find that, indeed, they have the same  $\gamma$  within our statistical noise. Of course, attending to Eq. (3),  $\Delta G_c$ , which depends only on  $R_c$  and  $\Delta p$ , is also the same for a given  $R_c$ , as illustrated in Fig. 7(c).

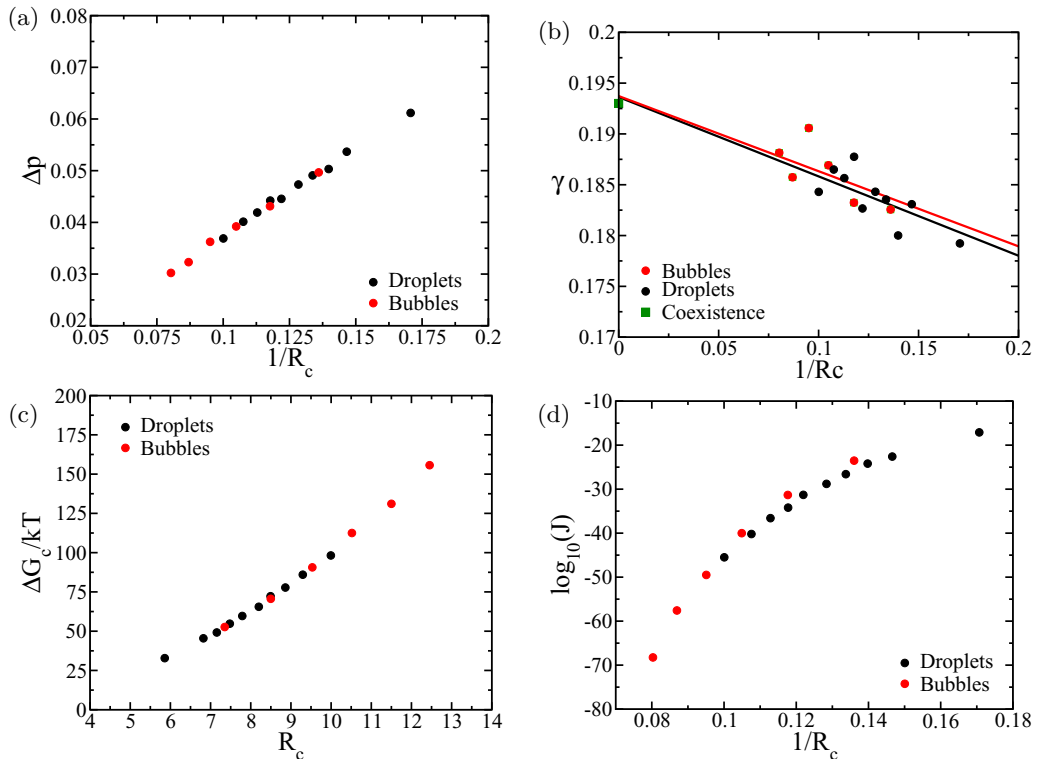


FIG. 7. (a)  $\Delta p$  vs  $1/R_c$ , (b)  $\gamma$  vs  $1/R_c$ , (c)  $\Delta G_c$  vs  $R_c$ , and (d)  $\log_{10} J$  vs  $1/R_c$  for droplets (black symbols) and bubbles (red symbols) as obtained from *NVT*-Seeding.



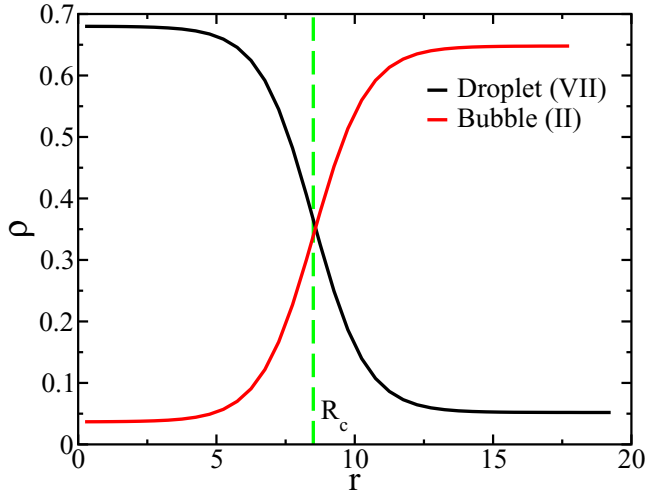


FIG. 8. Radial density profiles of drop VII and bubble II, compared. They have almost identical radius,  $R_c$ .

The nucleation rate for bubbles with a given  $R_c$  is close to the corresponding drop but is not exactly the same, given that the kinetic prefactor is not identical. In the case of bubble nucleation we have carefully assessed [70] that the following expression by Blander and Katz (BK) provides a good approximation for  $A_0$ :

$$A_0^{BK} = \sqrt{\frac{\Delta p R_c}{\pi m}}, \quad (16)$$

which is very similar, but with a missing  $(\rho_{\text{vap}}/\rho_l)$  factor with respect to the  $ktg$  expression we use for drop condensation [Eq. (10)]. The  $A_0^{BK}$  values we use in our Seeding predictions of bubble cavitation are reported in Table IV alongside the resulting values of  $J$  obtained as  $J = \rho_l A_0^{BK} \exp[-\Delta G_c/(k_B T)]$ . As can be seen in Fig. 7(d), the rate for bubbles and drops for a given  $R_c$  is quite similar, although it is systematically lower for the latter due to the  $\rho_{\text{vap}}/\rho_l$  factor previously mentioned.

Condensation and cavitation have already been compared in the literature [32,35,43,48,105–107]. However, there are only a few cases in which  $\gamma$  has been compared for a given temperature as a function of the droplet or bubble size [32,35] as we do in this work. Establishing such a comparison in experiments is difficult because it is not possible to detect the critical nucleus. In simulations the nucleus can be visualized, but computing  $\gamma$  is a hard task. It requires either computing the free energy of a system with the nucleus inside [32,34] or, more easily, computing the nucleus size and using a theory to infer  $\gamma$  [60,108] as we do in this work. In either approach, one has to deal with the arbitrariness of establishing a location for the interface.

In our case, we found in a recent work by “trial and error” that the equidensity surface gives good results for cavitation [70]. By “good results” we mean that Seeding predictions of nucleation are consistent with those coming from independent methods that do not rely on a precise definition of the nucleus size. In this work we have demonstrated that the same criterion to locate the interface is successful in condensation. Therefore, one of our main findings is that the equidensity surface is the one that provides good predictions

when CNT is used both for cavitation and for condensation. This means that the equidensity surface can be identified with the surface of tension, which is the one for which CNT works and the Laplace equation holds (see Sec. III) [47,49,55,109]. We believe that identifying the surface of tension with the equidensity surface for both cavitation and condensation is an important finding of our work. This leads to the relevant conclusion that condensation and cavitation are two sides of the same coin in the sense that they share the same surface tension.

In Ref. [35]  $\gamma$  was found to be quite different for both phenomena, but the comparison was not established for the surface of tension but for the equimolar surface. In Ref. [32], however, the comparison was established for the surface of tension, and, although  $\gamma$  was similar for condensation and cavitation, there were significant differences that need to be further investigated in order to match our work with that of Ref. [32].

### B. Comparison for a given metastability degree

In Ref. [83] it was proposed in a DFT study that the work of formation of critical bubbles studied at different temperatures collapses when plotted against the metastability degree,  $X_m$ , quantified as

$$X_m = \frac{\mu_{\text{nuc}} - \mu_{\text{coex}}}{\mu_{\text{spinodal}} - \mu_{\text{coex}}}, \quad (17)$$

where  $\mu_{\text{nuc}}$  is the chemical potential of the parent phase at the conditions where nucleation is studied,  $\mu_{\text{coex}}$  is the coexistence chemical potential at the same temperature and at coexistence pressure, and  $\mu_{\text{spinodal}}$  is the chemical potential at the same temperature but at the pressure where spinodal decomposition takes place. To estimate the spinodal pressure we run  $NpT$  simulations of the bulk liquid and vapor phases with 4000 particles. We estimate the spinodal decomposition pressure as that for which the system undergoes a phase transition without any induction period, right after the start of the simulation. Both chemical potential differences in Eq. (17) can be easily obtained by numerically integrating the molar volume along pressure at constant temperature. The denominator is the maximum possible metastability, whereas the numerator is the actual metastability of the state where nucleation is studied. Therefore,  $X_m$  varies from 0 at coexistence, to 1 at spinodal decomposition. The metastability degree above described can be computed for drop as well as for bubble nucleation. Therefore, we have the chance to compare nucleation free energy barriers for drops and bubbles as a function of  $X_m$ . The comparison, shown in Fig. 9, reveals the interesting conclusion that  $\Delta G_c$  for bubble and drop nucleation is the same for a given metastability degree. Therefore, not only can nucleation barriers at different temperatures be collapsed via the metastability degree as proposed in Ref. [83], but bubble and drop nucleation data also match for a given metastability degree.

### C. Tolman length

Since bubbles and drops of the same radius have the same interfacial properties, we can use the data coming from both

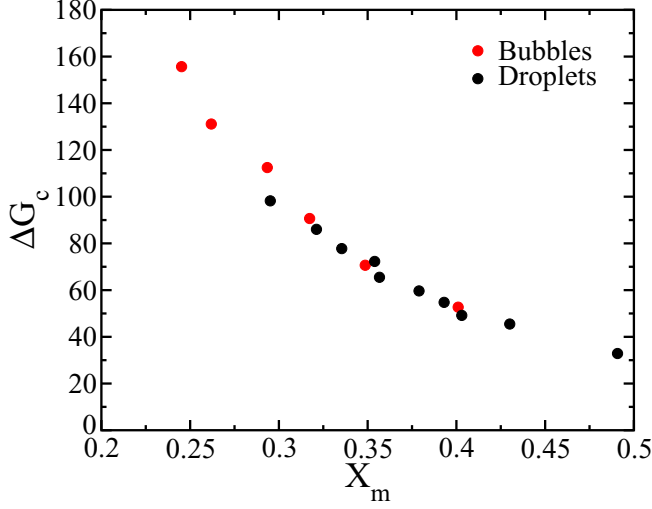


FIG. 9. Nucleation free energy barrier for drops and bubbles (see legend) as a function of the metastability degree,  $X_m$ , defined in Eq. (17).

systems altogether in order to compute the Tolman length,  $\delta_T$ , which is defined as [34,74]

$$\delta_{\text{Tolman}} = \lim_{R_s \rightarrow \infty} (R_e - R_s), \quad (18)$$

where  $R_e$  is the Gibbs equimolar radius and  $R_s$  is the radius of the surface of tension. We identify  $R_s$  with  $R_c$  (the equidensity radius) given that (1) we obtain good predictions of nucleation when we use  $R_c$  and (2)  $R_s$  is the radius that enters CNT [47,49,55,109]. To underline the fact that we identify  $R_c$  with  $R_s$  we label  $R_c$  as  $R_{s=c}$  in the following figures.  $R_e$  can be easily computed from the radial density profiles [54,55]. In Fig. 10(a) we show  $R_e - R_{s=c}$  versus  $1/R_{s=c}$  for all data (either bubbles or drops) coming from this work. The extrapolation to  $1/R_{s=c} = 0$  provides an estimate of  $\delta_{\text{Tolman}}$ , indicated with an empty blue dot in the figure. We obtain  $\delta_{\text{Tolman}} = 0.15 \pm 0.02$ . We showed in a recent paper, in which we analyzed spherical hard sphere crystals in equilibrium with the fluid, that  $\delta_{\text{Tolman}}$  can be also estimated by fitting  $\gamma$  to the following expression:

$$\gamma = \gamma_0 \left( 1 - 2 \frac{\delta_T}{R_s} \right), \quad (19)$$

where  $\gamma_0$  is the value of  $\gamma$  at coexistence at the temperature of interest and  $\delta_T$  is the fitting parameter that serves as an estimate for  $\delta_{\text{Tolman}}$  [55]. This approach is similar in spirit to those that include  $\gamma$  given by Eq. (19) in CNT to fit free energy barriers obtained by rare event methods [84,110]. Again, we identify here  $R_s$  with  $R_c$ . Consequently, we use the  $\gamma$  data coming from such a radius (that reported in Tables I and IV) to obtain an estimate of  $\delta_T$  with the expression above. The data of  $\gamma$  versus  $1/R_{s=c}$  are shown in green in Fig. 10(b). The solid line is a linear fit of  $\gamma$  versus  $1/R_{s=c}$ , which includes  $\gamma_0$  (the green square in the figure). The  $\delta_T$  value coming from such fit,  $\delta_T = 0.21 \pm 0.03$ , is shown with a red dot in Fig. 10(a). Both values,  $\delta_{\text{Tolman}}$  obtained via Eq. (18) [blue dot in Fig. 10(a)] and  $\delta_T$  coming from Eq. (19) (red dot in the same figure), are consistent with each other within the statistical uncertainty of our estimates. This corroborates the idea, recently checked

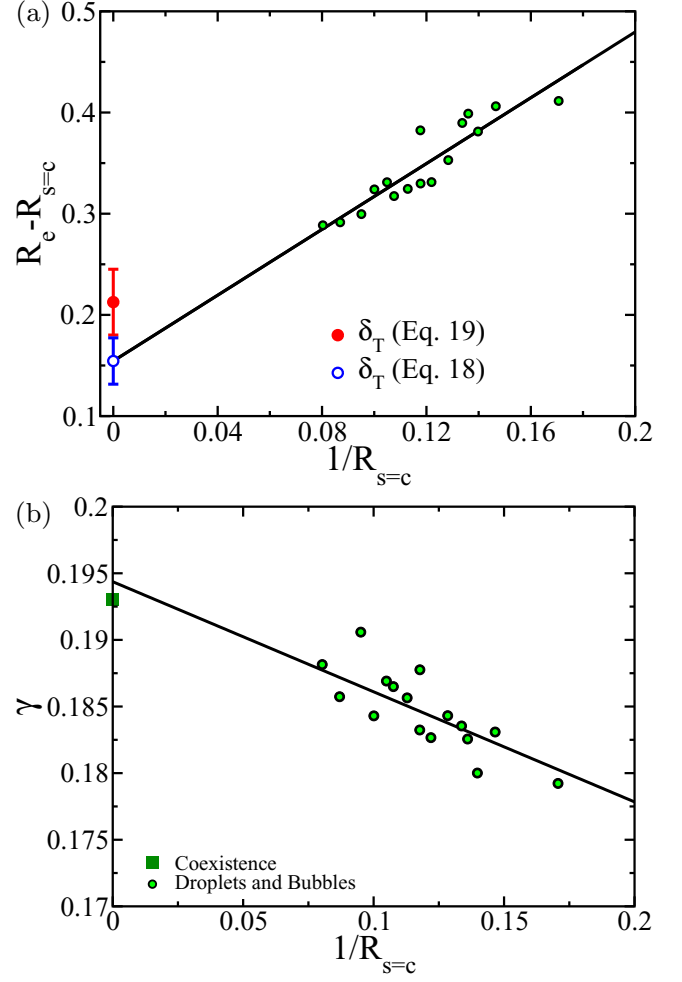


FIG. 10. (a)  $R_e - R_{s=c}$  and (b)  $\gamma$  vs  $1/R_{s=c}$  for drops and bubbles together.

for hard sphere crystals [55], that the Tolman length can be obtained either from Eq. (19) or from Eq. (18). Hence, this idea seems to be a general one pertaining not only to the crystal-fluid equilibrium but also to the liquid-vapor one.

This study may shed some light in the intense literature debate about the magnitude and sign of the Tolman length [18,30–32,34–44]. We obtain a Tolman length of about 20% of the particle diameter. Its sign is positive, which means that  $\gamma$  decreases when one moves away from coexistence at constant temperature.

## VI. CONCLUSIONS

The main conclusions we draw from our work are the following:

(1) We have used *NVT-Seeding* to investigate droplet nucleation in a supersaturated Lennard-Jones vapor. The results obtained from this technique are consistent with the following: (i) independent calculations of the nucleation free energy barrier performed with Umbrella Sampling, (ii) the surface tension of a flat interface obtained from the pressure tensor in a vapor-liquid coexistence simulation, and (iii) the drop

nucleation rate obtained both with US and in brute force spontaneous nucleation simulations.

(2) *NVT*-Seeding requires defining the radius of a droplet equilibrated in the *NVT* ensemble. The radius definition that passes the consistency tests mentioned in point (1) is that given by the surface where the density is average between that of the interior and that of the exterior phases. Such a radius definition was also successful in our earlier studies of bubble nucleation [54,70]. Therefore, we identify this “equidensity” radius with the radius of tension,  $R_s$ .

(3) The good performance of Seeding strongly supports the use of CNT to describe nucleation. However, the capillarity approximation (that  $\gamma$  is curvature independent) does not provide good results. A  $\gamma$  dependent on the curvature of the critical nucleus must be plugged into the theory. Therefore, the theory, although powerful, requires the involvement of simulations given that the  $\gamma$ -curvature dependence is obtained by computing the size of the critical cluster at different pressures.

(4) The kinetic theory of gases provides very good estimates of the kinetic prefactor of the condensation nucleation rate. This makes the theoretical framework very powerful given that only the size of the critical cluster, the density of the external phase, and the bulk phases equations of state are needed to estimate nucleation rates.

(5) We compare *NVT*-Seeding results of droplets with those obtained for bubbles and find that, for a given

temperature, bubbles and droplets of the same radius have, within the accuracy of our method, the same pressure difference with the surrounding medium. Therefore, bubbles and droplets of the same size have the same surface tension and the same nucleation free energy barrier. In this respect, condensation and boiling can be seen as two sides of the same coin. Such duality is verified only if the size of the critical nucleus (either a bubble or a drop) is determined with the equidensity radius (our empirical definition of the surface of tension).

(6) We estimate the Tolman length,  $\delta_T$ , by extrapolating to infinite-size drops and bubbles the difference between the equimolar radius,  $R_e$ , and  $R_s$ . Such  $\delta_T$  is consistent with that obtained by linearly fitting  $\gamma(1/R_c)$ , in accordance with our recent work on hard sphere crystals [55].

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